

# Development of mathematical modelling tool for analysis and optimization of the High Temperature Solid Oxide Steam Electrolysis process

## STARRING

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# Hydrogen production

## Utilization

- Chemical industry
- Hydrogen economy

## Production methods

- Steam reforming
- Water electrolysis
  - Minor
  - Sustainable
  - Pure
  - Electric energy storage/consumption



Alkaline water electrolysis

# Water electrolysis

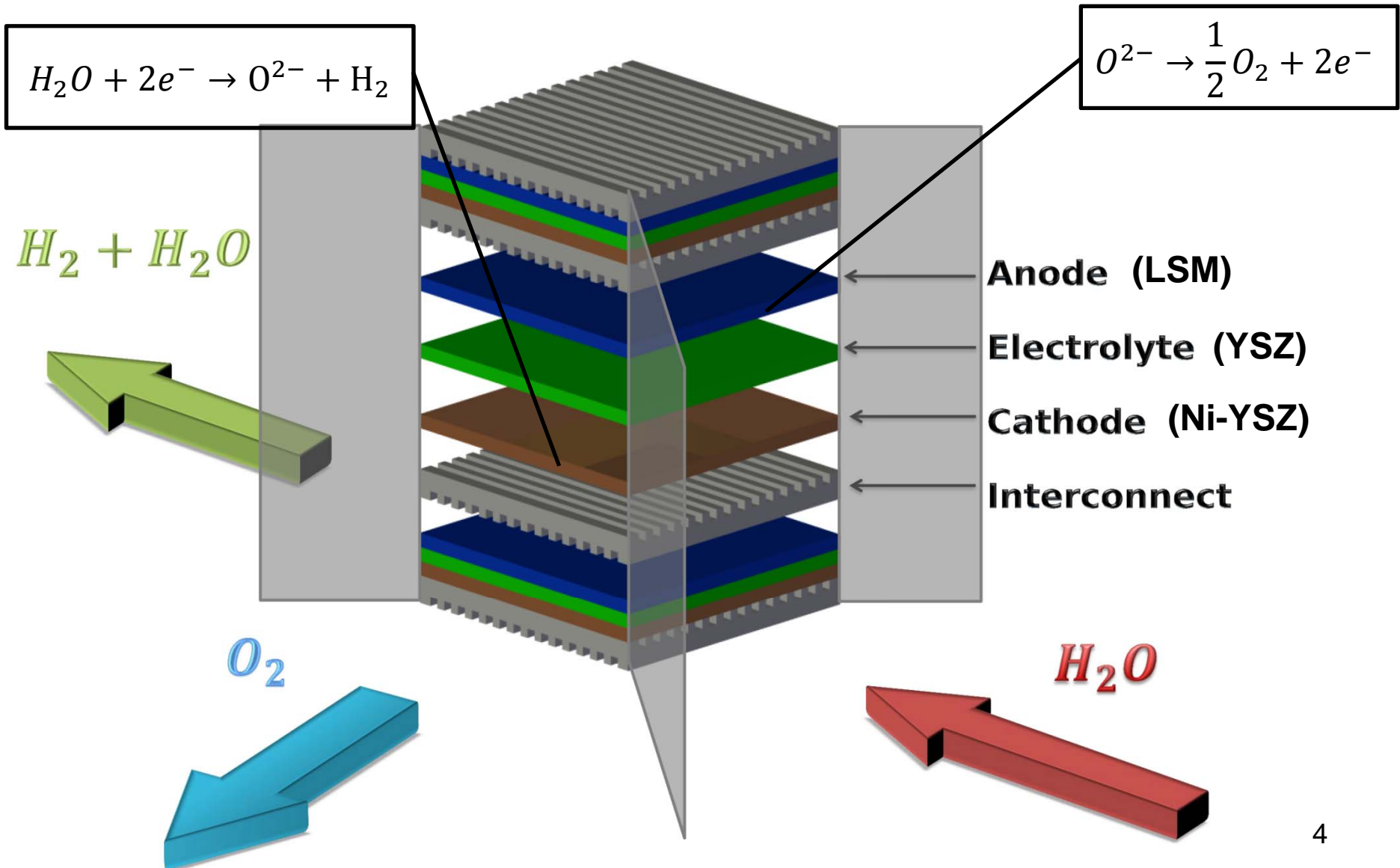
## Conventional

- Alkaline Water Electrolysis
- High electric energy requirement

## Alternative

- High Temperature Steam Electrolysis
- Lower electric energy input
- Economical only with appropriate heat source  
(cheap, stable, high temperature)

## HTSE - planar arrangement



# Objectives

## Long-term goals

- Mathematical modeling the HTSE process
  - Understanding
  - Prediction
  - Optimization
  - Scale-up

## Presentation objectives

- History and current stage of development in ICTP
- Peculiarities of HTSE system

# Mathematical background

## Charge transfer

$$\nabla \cdot \mathbf{j}_{io} = \nabla \cdot (-\sigma_{io} \nabla \Phi_{io}) = \mathbf{j}_R \cdot \mathbf{a}_{TPB}$$

$$\nabla \cdot \mathbf{j}_{el} = \nabla \cdot (-\sigma_{el} \nabla \Phi_{el}) = -\mathbf{j}_R \cdot \mathbf{a}_{TPB}$$

$$\mathbf{j}_R = \mathbf{j}_0 \left( \frac{c_{red}}{c_{red}^*} e^{\beta_{ox} \eta \frac{zF}{RT}} - \frac{c_{ox}}{c_{ox}^*} e^{-\beta_{red} \eta \frac{zF}{RT}} \right)$$

## Heat transport

$$\nabla \cdot (\vec{\hat{h}} + \vec{\hat{q}}) = \nabla \cdot (c_p \vec{\hat{n}} T - \lambda \nabla T) = q_R$$

# Mathematical background

## Material transport - porous structures

$$\nabla \cdot \vec{\hat{n}}_{\text{H}_2\text{O}} = \nabla \cdot (-D_{\text{H}_2\text{O}} \nabla p_{\text{H}_2\text{O}}) = n_{\text{R,H}_2\text{O}} \cdot a_{\text{TPB}}$$

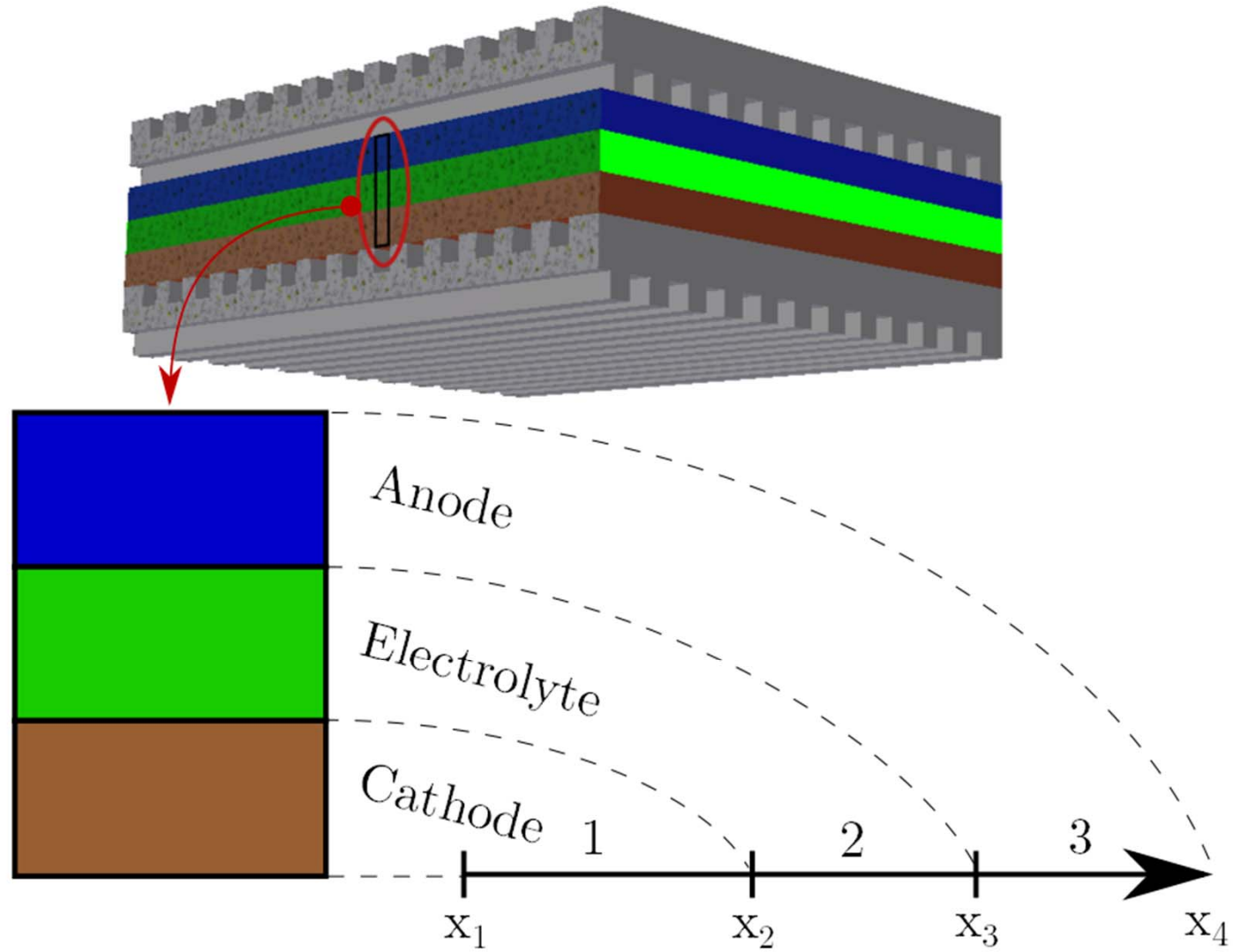
$$\nabla \cdot \vec{\hat{n}}_{\text{O}_2} = \nabla \cdot (-D_{\text{O}_2} \nabla p_{\text{O}_2}) = n_{\text{R,O}_2} \cdot a_{\text{TPB}}$$

$$p_{\text{H}_2} = p - p_{\text{H}_2\text{O}}, \quad D^{\text{eff}} = \frac{\varepsilon}{\xi} \left( \frac{1}{D_{\text{Knudsen}}} + \frac{1}{D_{\text{Transport}}} \right)^{-1}$$

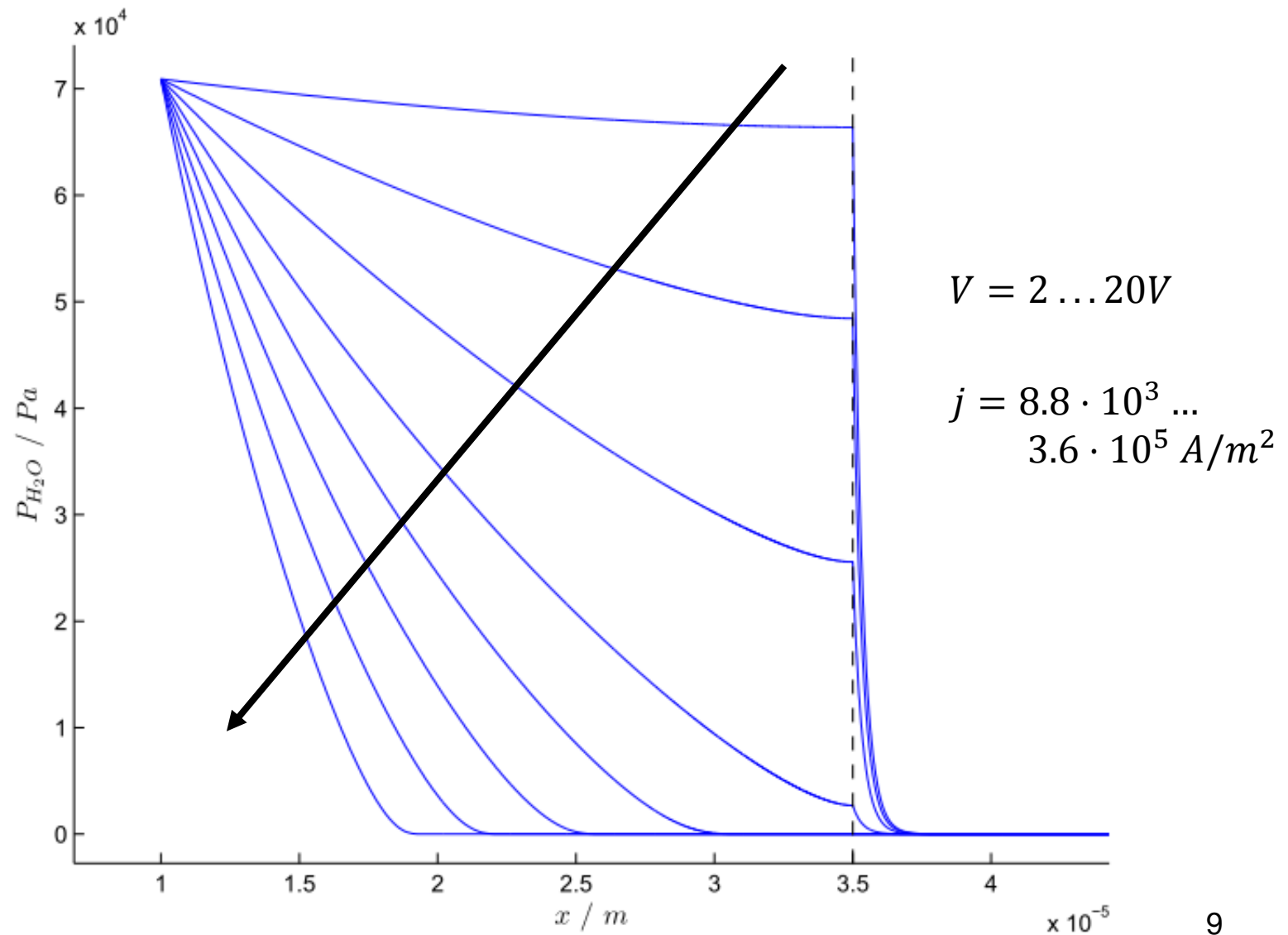
## Material transport – flow channels

- Navier-Stokes equation (laminar flow)
- Continuity equation (compressible)

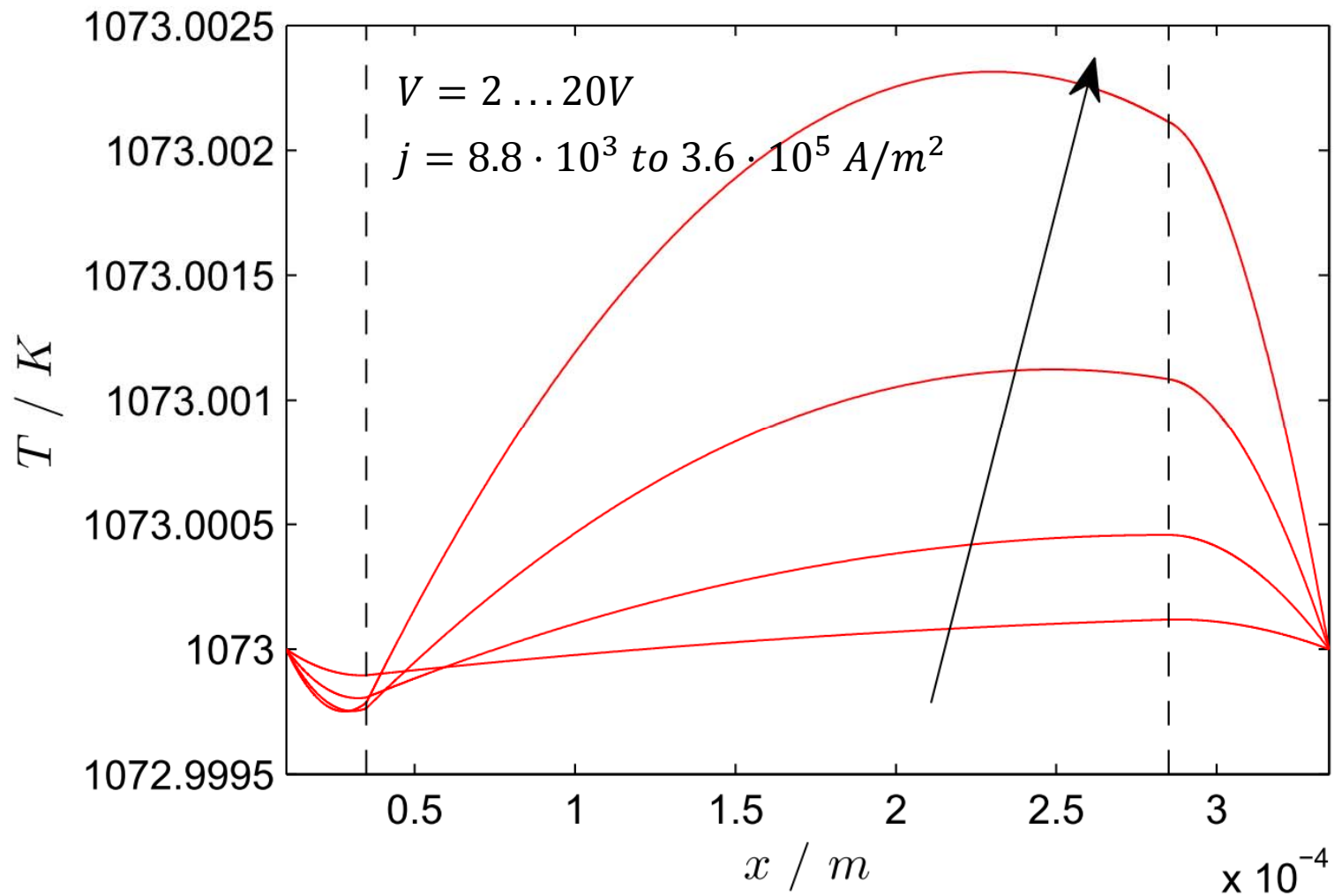
# 1D modelling



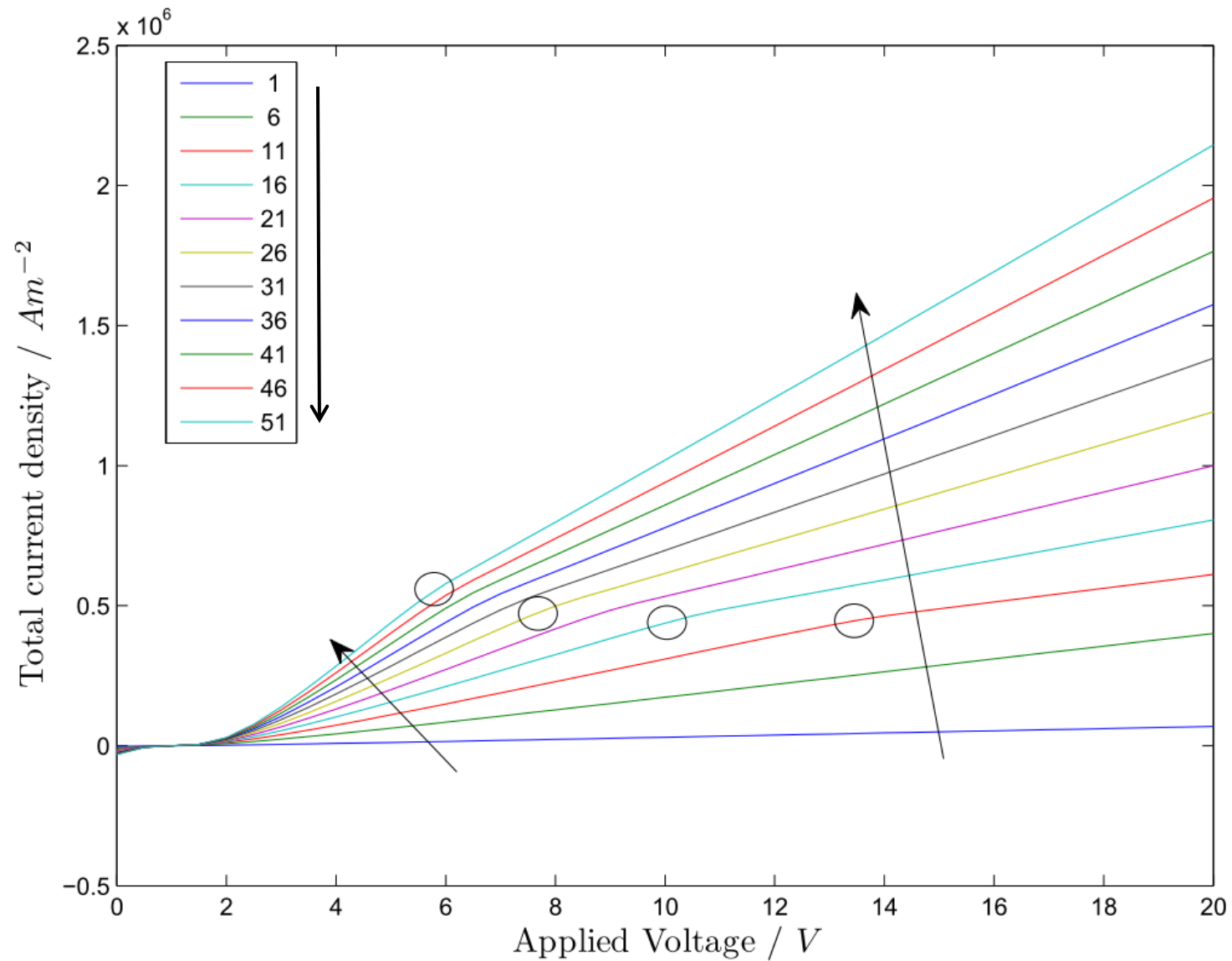
# 1D modelling



# 1D modelling – temperature

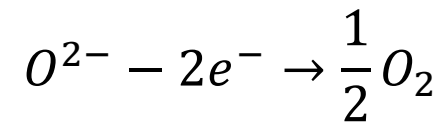
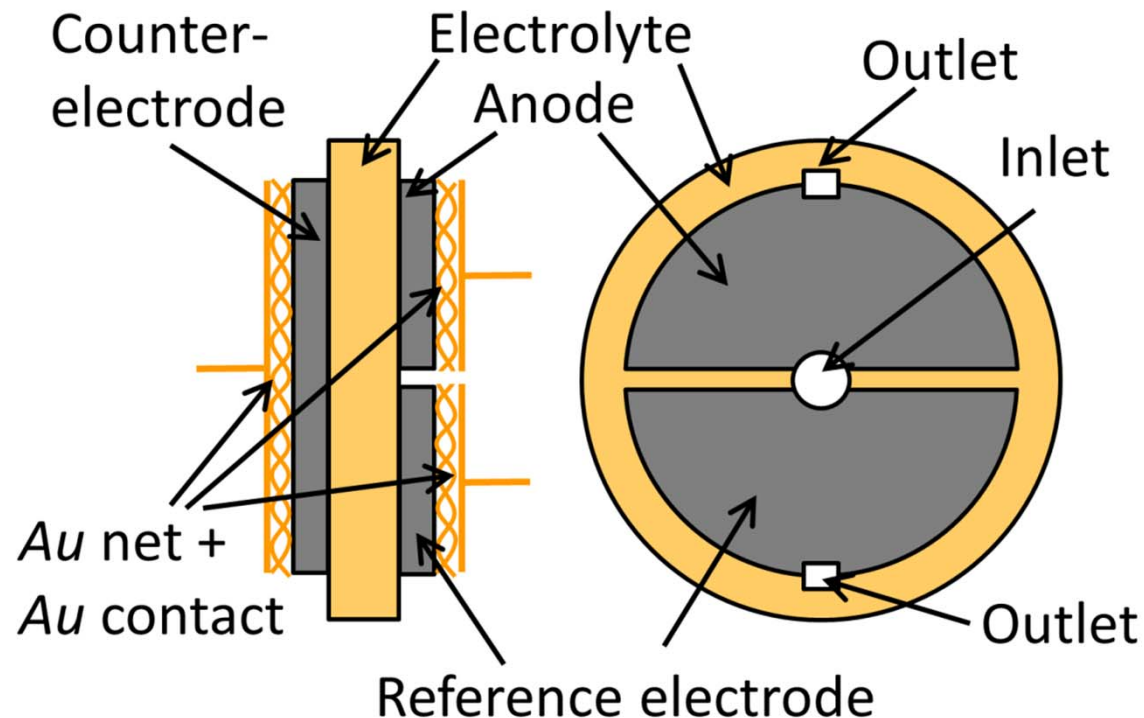


# 1D modelling – YSZ conductivity



# Evaluation of kinetic data of anode reaction

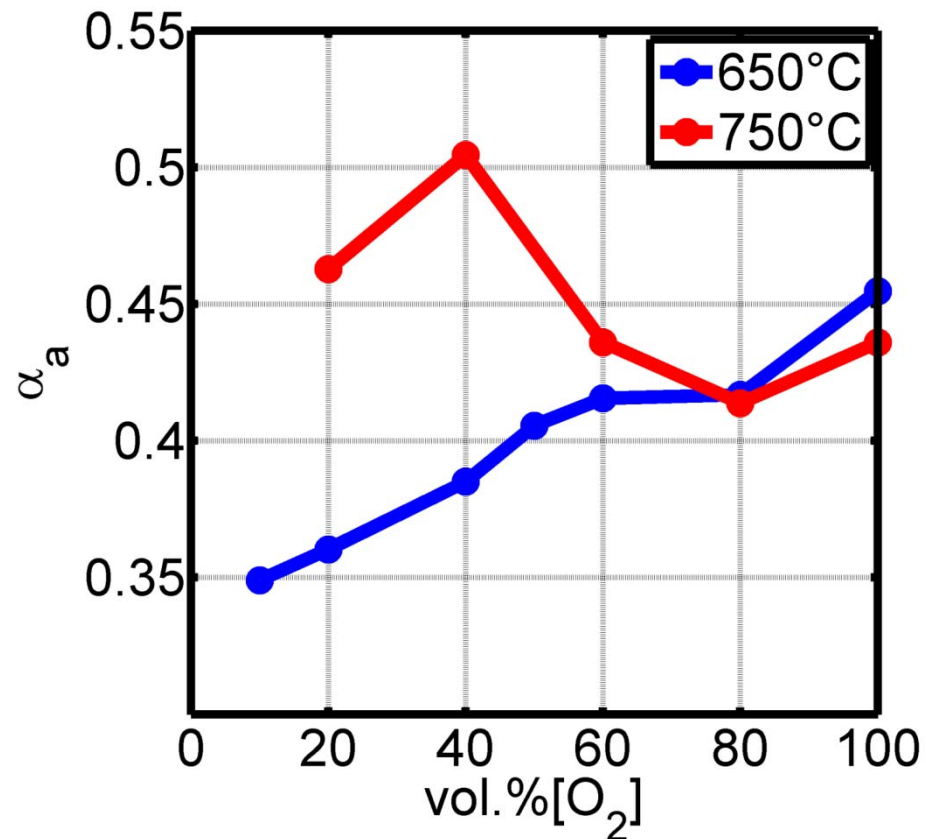
- 1st step: potentiodynamic measurements of LSM anode in symmetric cell



**Anode/Reference electrode:**  $O_2 + N_2$ , 20-100 vol.%[ $O_2$ ], **Counter electrode:** air  
**Temperature** 650 °C, 750 °C, **Pressure:** atmospheric

# Evaluation of kinetic data of anode reaction

- 2nd step: Tafel analysis of anodic region of overvoltage



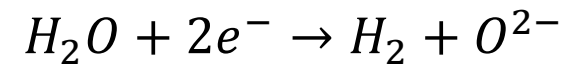
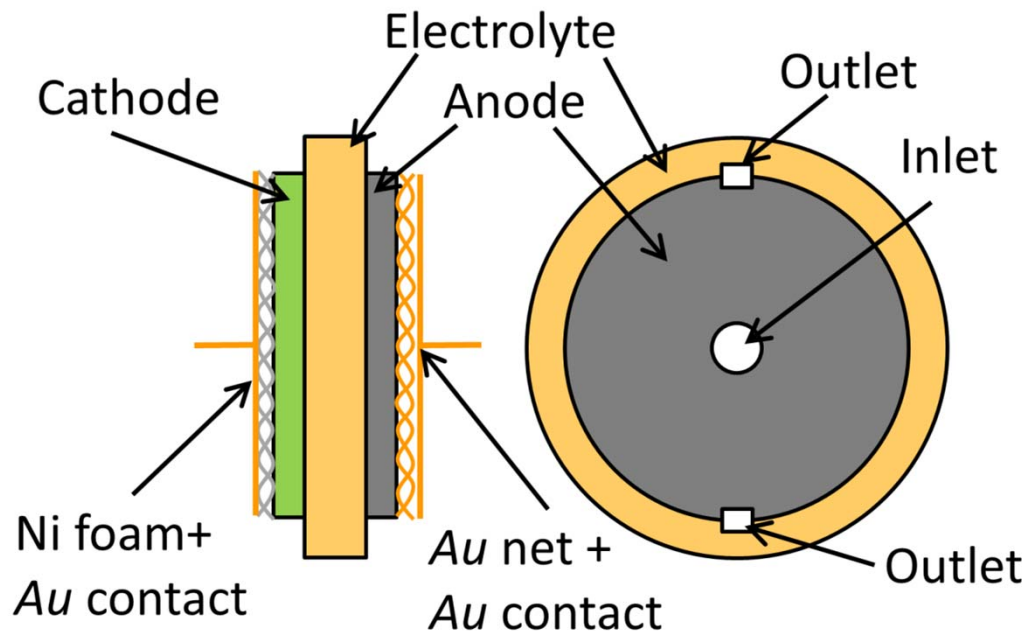
Tafel's equation

$$\eta = -\frac{RT}{\alpha_a F} \ln(I_{o,a}) + \frac{RT}{\alpha_a F} \ln(I)$$

60 vol.%[O<sub>2</sub>]  
750 °C

# Evaluation of kinetic data of cathode reaction

- 1st step: measurements of current density – voltage curves on an experimental HTSE cell



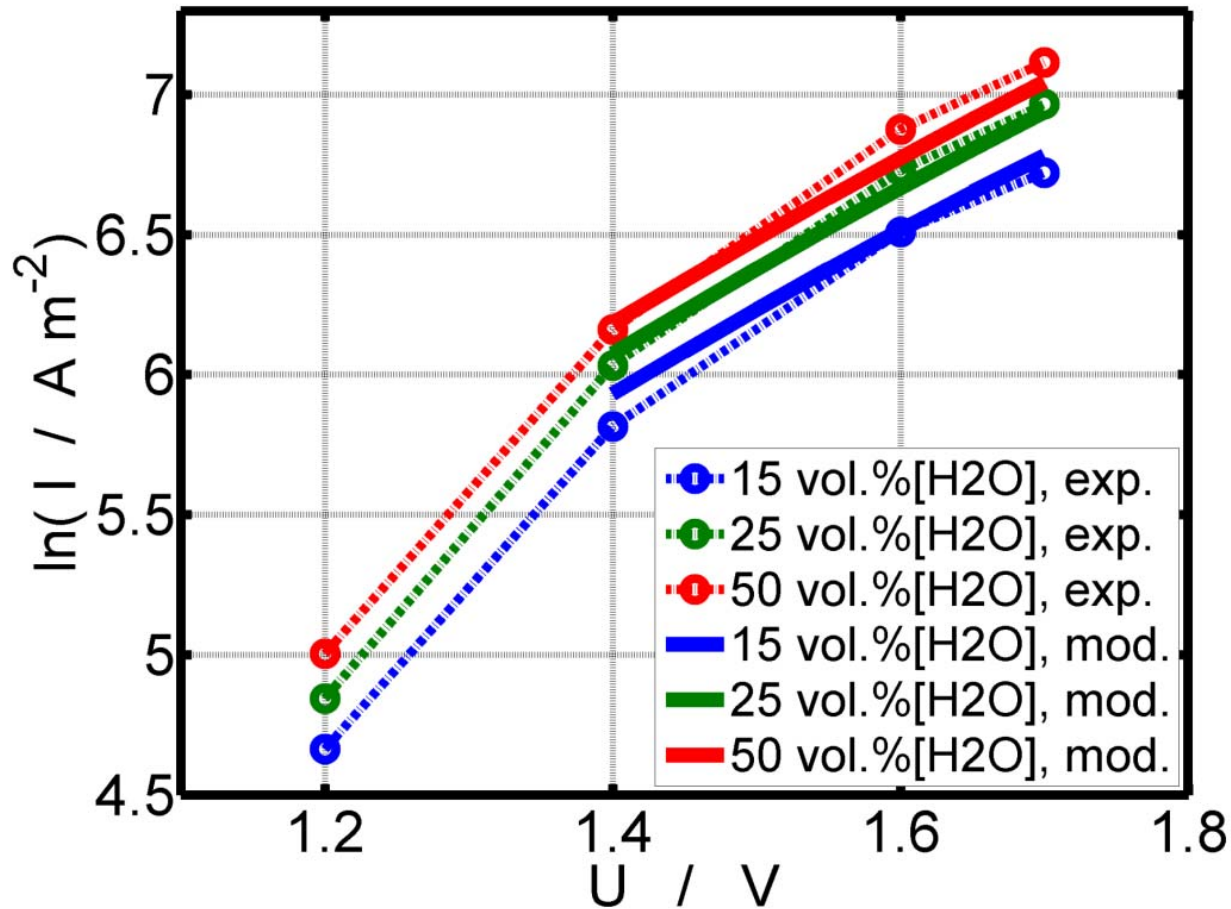
**Temperature 800 °C; Pressure atmospheric;  
Anode: air, Cathode: H<sub>2</sub>O+H<sub>2</sub>; 15, 25 and 50 vol. %[H<sub>2</sub>O]**

# Evaluation of kinetic data of cathode reaction

- 2nd step: development of a Pseudo-2D model of HTSE cell having two fitting kinetic parameters  $\alpha_c$  and  $I_{0,c}$
- Cylindrical symmetry - coordinate is  $r$  (radius) oriented from center to the cell perimeter
- Electric current flow normal to cell plane
- Stationary, isobaric, isothermic (800 °C)

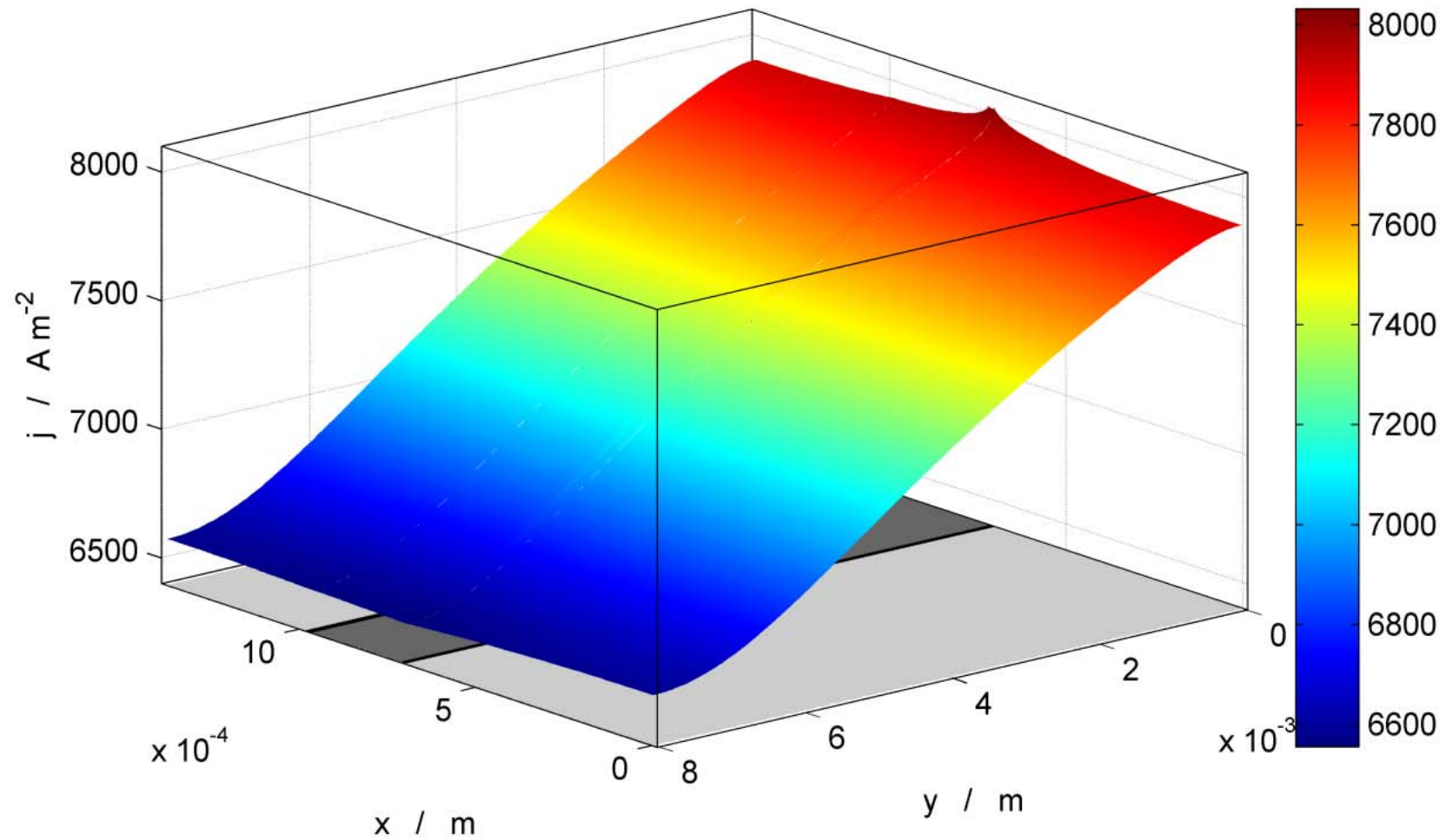
$$U = U_{OCV} - \left( \frac{RT}{\alpha_a F} \ln(I_{o,a}) + \frac{RT}{\alpha_c F} \ln(I_{o,c}) \right) + \\ + \left( \frac{RT}{\alpha_a F} + \frac{RT}{\alpha_c F} \right) \ln(I) + \frac{RT}{\alpha_c F} \ln \left( \frac{p_{H_2O}}{p^0} \right) + R_{s,cell} I$$

# Evaluation of kinetic data of cathode reaction



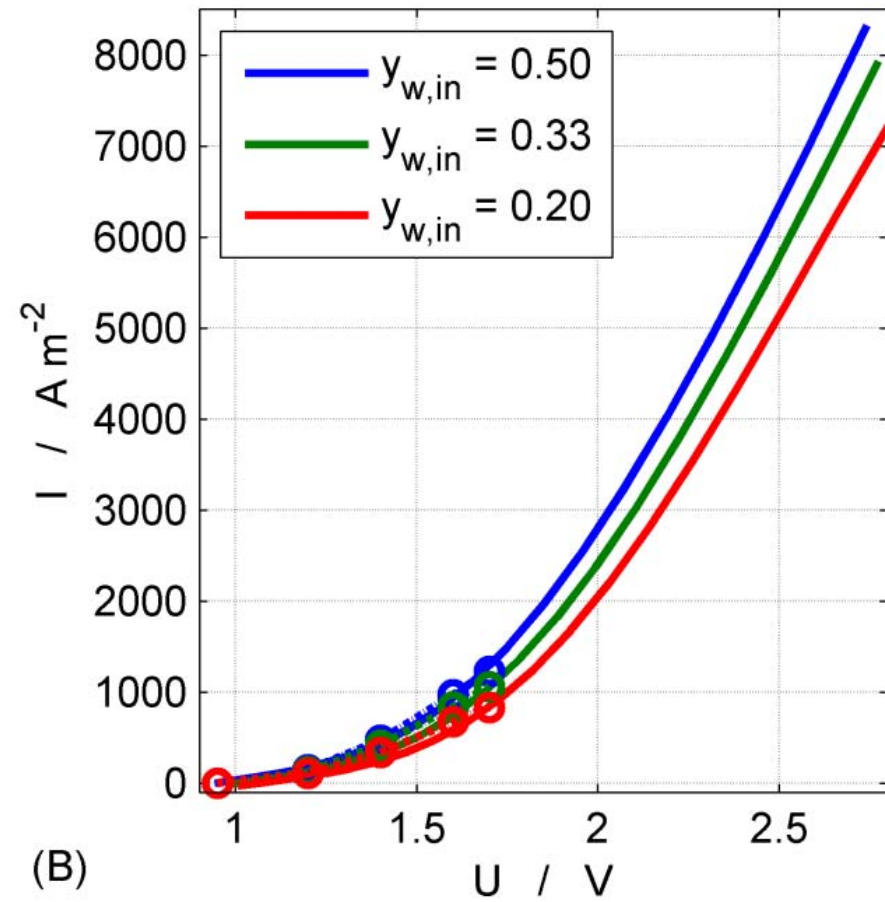
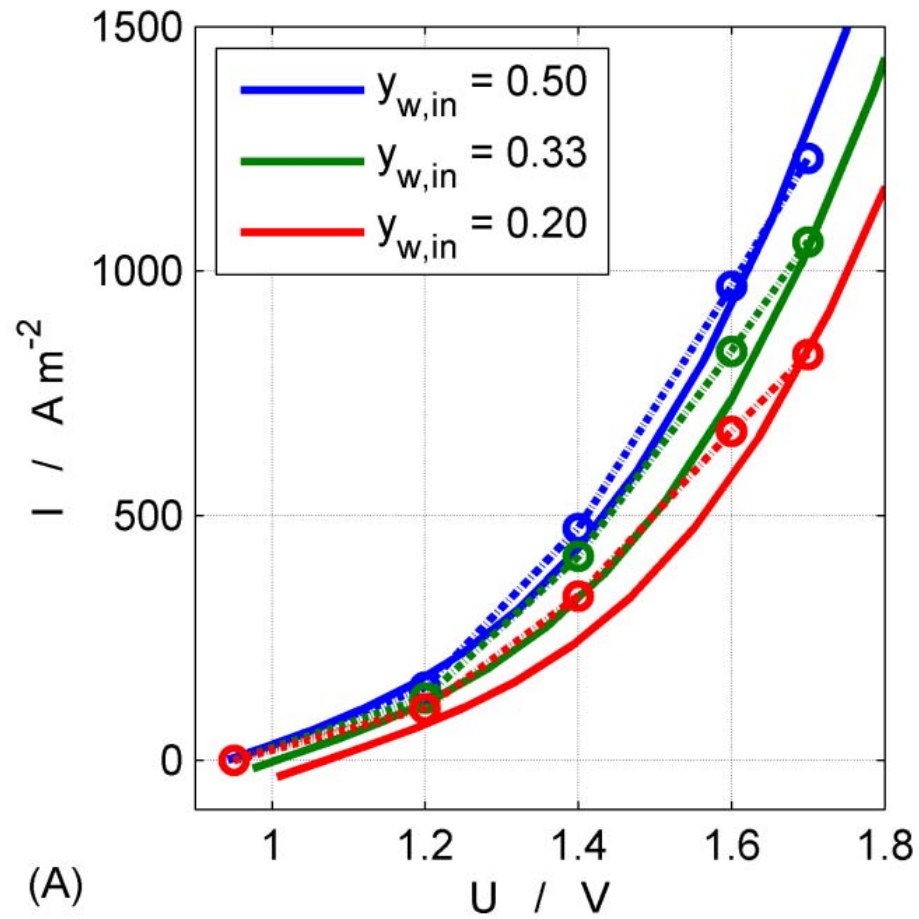
$\alpha_a = 0.45$  (750°C), 0.40 (650°C);  $I_{o,a} = 15.03 \text{ A m}^{-2}$  (750°C),  $8.14 \text{ A m}^{-2}$  (650°C);  
 $\alpha_c = 1.19$  (800°C);  $I_{o,c} = 4.79 \text{ A m}^{-2}$  (800°C)

## 2D modelling



$T = 800\text{ }^{\circ}\text{C}$ ,  $y_{w,in} = 0.2$ ;  $U = 2.8\text{ V}$ ;  $I = 7249\text{ A m}^{-2}$

## 2D modelling



$T = 800 \text{ } ^\circ\text{C}$